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(NASA-CR-165457-Vol-2-Pt-1) AN EXPERIMENTAL N82-18180 INVESTIGATION OF GAPWISE PERIODICITY AND HC ALL MF AOI UNSTEADY AERODYNAMIC RESPONSE IN AN HC ALL UNCLASE REPORT. PART (United Technologies Research G3/02 09158

NASA Contractor Report 165457 - Part 1 of 2 (UTRC Report R81-914618-28)

AN EXPERIMENTAL INVESTIGATION OF GAPWISE PERIODICITY AND UNSTEADY AERODYNAMIC RESPONSE IN AN OSCILLATING CASCADE VOL. II: DATA REPORT

(Part 1: Text and Mode 1 Data)

F. O. Carta

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the unsteady pressure response cascade, over the chord of the leading edge. The tests were coincidence angles ($\alpha_{\rm MCL}=2$ and reduced frequencies ($k=.072$, phase angles ($\sigma=0,\pm45,\pm90$) Fourier coefficient form for dintegrated loads and, particular	on selected blades along the center blade, and on the side conducted for all 96 combinati 6 deg), 2 pitching amplitudes .122, and .151 based on semi 1, ± 135, 180 deg). The press rect comparison, and were alsorly, the aerodynamic damping of this program are presented cribes the test procedure, dicursory comparison of experis	wall in the plane of the cons of 2 mean camberline (\alpha = 0.5 and 2 deg), 3 chord), and 8 interblade course data were reduced to co processed to yield coefficient. in two volumes. The scusses key results from mental data and theoretical
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SUMMARY

Tests were conducted on a linear cascade of airfoils oscillating in pitch to measure the unsteady pressure response on selected blades along the leading edge plane of the cascade, over the chord of the center blade, and on the sidewall in the plane of the leading edge. The tests were conducted for all 96 combinations of 2 mean camberline incidence angles ($\alpha_{\rm MCL} = 2$ and 6 deg), 2 pitching amplitudes ($\alpha = 0.5$ and 2 deg), 3 reduced frequencies (k = .072, .122, and .151 based on semi chord), and 8 interblade phase angles ($\sigma = 0$, \pm 45, \pm 90, \pm 135, 180 deg). The pressure data were reduced to Fourier coefficient form for direct comparison, and were also processed to yield integrated loads and, particularly, the aerodynamic damping coefficient.

The experimental results of this program are presented in two volumes. The first volume (Ref. 1) describes the test procedure, discusses key results from the experiment, and provides a cursory comparison of experimental data and theoretical predictions. The present volume, in two parts, is a compilation of all data obtained during the test program, reproduced from the printout of the data reduction program. A further description of the contents of this report is found in the text that follows.

LIST OF SYMBOLS

Note: In this tabulation the first column is the heading from the computer printout reproduced herein, the second column is the equivalent physical symbol defined in Ref. 1, and these are followed by a brief definition.

Symbol in this report	Symbol in Ref. 1	Definition
ALPHA-BAR	ā	pitching amplitude, deg
ALPHA-MCL	^α mcl	mean camberline incidence angle, deg
CMIMAG	$\mathbf{c}_{_{\mathbf{M_{I}}}}$	imaginary part of moment coefficient per unit amplitude
CMREAL	$^{\mathrm{c}}_{_{\mathrm{M}_{\mathrm{R}}}}$	real part of moment coefficient per unit amplitude
CM-MAG	$\overline{\mathbf{c}}_{\mathtt{M}}$	magnitude of moment coefficient per unit amplitude
CNIMAG	$^{\mathrm{C}}{}_{\mathrm{N}}{}_{\mathrm{I}}$	imaginary part of normal force coefficient per unit amplitude
CNREAL	$\mathbf{c_{N}}_{R}$	real part of normal force coefficient per unit amplitude
CN-MAG	$\overline{c}_{_{ extbf{N}}}$	magnitude of normal force coefficient per unit amplitude
CPIMAG	c^b ^I	imaginary part of single surface pressure coefficient per unit amplitude
CPREAL	c _p R	real part of single surface pressure coefficient per unit amplitude
CP-MAG	¯c _p	magnitude of single surface pressure coefficient per unit amplitude
DELCPI	$^{\Delta C_{\mathbf{p}}}$ I	imaginary part of pressure difference coefficient per unit amplitude
DELCPM	ΔCp	magnitude of pressure difference coefficient per unit amplitude
DELCPR	$\Delta c_{\mathbf{p}_{\mathbf{R}}}$	real part of pressure difference coefficient per unit smplitude

LIST OF SYMBOLS (Cont'd)

Symbol in this report	Symbol in Ref. 1	Definition
FILE	-	internal file number, used for computer access
К	' k	reduced frequency
n	k	harmonic number
PHI	ф	phase angle lead relative to motion
PHIM	$\phi_{\mathbf{M}}$	moment phase angle lead relative to motion
PHIN	$\phi_{\mathbf{N}}$	normal force phase angle lead relative to motion
PDP RUN.PT	ānis	internal computer reference number
POINT	a -c	point number assigned during test
Q-COMP	q	dynamic pressure
RUN	•••	run number assigned during test
SIGMA	σ	interblade phase angle
V-REF	v	reference velocity at blade 6
x	x	dimensionless distance along chord
XI	[2]	aerodynamic damping parameter

Supplementary Notes:

- All pressures are normalized with respect to Q-COMP = q and ALPHA-BAR = α (in radians)
- The notation UPPER or LOWER in MODE 1 refers to the blade surface and pertains to the column of numbers beneath this notation
- The notation SUCTION or PRESSURE in MODE 2 refers to the blade surface and pertains to the tabulations to the right of this notation
- UPPER = SUCTION, LOWER = PRESSURE
- The values set equal to X * X are the chord Practions at which the measurements were made
- Imaginary part is out of phase and real part is in phase with the pitching motion.

DISCUSSION

The experimental procedures used and the results obtained from this program are both fully described in the companion technical report volume (Ref. 1). The objective of this data report is to provide full documentation for this experiment, in the form of reproduced computer printout of the data reduction program. However, for completeness, a brief description of the test program, model airfoils, and instrumentation will be included.

Oscillating Cascade Wind Tunnel

The experimental program was carried out in the UTRC linear subsonic Oscillating Cascade Wind Tunnel (OCWT). The test section of this facility is 25.4 cm (10 in) wide and 68.6 cm (27 in) high, and the sidewall configuration is currently arranged to accept 11 shaft-mounted blades in cascade. The bearing mounts for these blades are equally placed along a line making a 30 deg angle with respect to the tunnel floor, and hence the sidewall stagger angle of the OCWT is nominally 30 deg. The distance between blade shaft centers along the stagger line is 11.43 cm (4.5 in).

Test Airfoils

The cascade configuration consists of eleven NACA 65-series blades, each having a chord of c = 15.24 cm (6 in) and a span of 25.4 cm (19 in), with a 10 degree circular arc camber and a thickness-to-chord ratio of 0.06. The slant gap, measured along the blade-to-blade stagger line, is $\tau = 11.43$ cm (4.5 in) so the gap-to-chord ratio is $\tau/c = 0.75$.

For these tests the blade stagger angle, β_1^* , measured between the tangent to the blade mean camber line at the leading edge and the leading edge locus line, is 30 deg. The blade inlet angle, β_1 , is measured between the inlet velocity, V, and the leading edge locus line. Hence, the mean camber line incidence angle is defined as $\alpha_{\text{MCL}} = \beta_1^* - \beta_1$. The blade profile coordinates, in fraction of chord, are contained in Table 1. The entire set of airfoils is coherently driven in a sinusoidal pitching motion with an amplitude of $\overline{\alpha}$.

Instrumentation

Conventional pneumatic wind tunnel instrumentation is used to measure the flow properties in the test section. A pitot probe downstream of the inlet honeycomb measures the total pressure in the tunnel, and sidewall static taps, aligned with the sidewall stagger angle, are used to measure the static pressure along the inlet and exit planes of the cascade. Tunnel speed is set by measuring the inlet plane static pressure at tunnel midheight and referring it to the pitot pressure to calculate the dynamic pressure, q.

The center airfoil (blade no. 6) was extensively instrumented to provide measurements of several flow parameters. Ten miniature high response pressure transducers were placed on each surface of the airfoil to obtain measurements of unsteady static pressures. This blade is shown schematically in Fig. 1.

Five other blades were also instrumented with miniature transducers. The blades are located in the cascade as shown in the schematic diagram in Fig. 2. Blade no. 6 is the fully instrumented center blade. Partial instrumentation was placed on blades no. 3, 4, 5, 7, and 9. Locations, in chord fraction, χ , of all transducer orifices are listed for all blades in Table 2a. As shown, blades 3, 5, 7, and 9 have suction surface orifices at χ = .0120, and .0622, and pressure surface orifices at χ = .0120 and .0622 and has additional suction surface orifices at χ = .0050 and .0350 with no orifice on the pressure surface.

Finally, an array of ten miniature transducers were mounted in the tunnel sidewall in the plane of the blade leading edges, as shown schematically in Fig. 3. (For simplicity these locations are depicted as being slightly forward of the leading edge plane although they were actually coincident with the plane.) The gap fraction location, η , of each transducer relative to the suction surface of blade 6 is listed in Table 2b.

Test Plan

A total of 96 test conditions were run. These were comprised of all possible combinations of two mean camber line incidence angles ($\alpha_{MCL} = 2$ deg, 6 deg), two pitching amplitudes ($\alpha = 0.5$, 2 deg) three frequencies (f = 9.2, 15.5, 19.2 Hz, and, for a constant velocity of 61 m/sec, or 200 ft/sec, this was equivalent to reduced frequencies $k = c\omega/2V = \pi cf/V = .072, .122, .151)$ and eight interblade phase angles ($\sigma = 0$ deg, ± 45 deg, ± 90 deg, ± 135 deg, 180 deg). In addition, two deta runs were taken at each test condition. This was necessary because the number of desired data locations (47) exceeded the number of available data system channels (26). Hence, a relay was employed to switch between Mode 1, which contained all twenty blade-6 channels, five wall channels, and blade motion, and Mode 2, which contained all nineteen blade leading edge charmels, six wall channels, and blade motion. Redundancy between modes was confined to the three leading edge stations on blade 6, one sidewall station, and blade motion. A tabulation of all data channels for each mode is contained in Table 3. In this table, the blade location is coded by a three symbol array denoting blade number, suction or pressure surface, and location sequence from leading edge. Wall stations are numbered consecutively. The numerical value for each location is either blade chord fraction, χ , or sidewall gap fraction, n.

Unsteady Data

The acquisition rate for all unsteady data was set at 1000 samples/sec. Thus, for the three nominal test frequencies, f = 9.2, 15.5, 19.2 Hz, there were 9.4, 15.9, and 19.7 cycles of data available for analysis, or conservatively, there were 9, 15, and 19 full cycles available. Data for each channel were Fourier analyzed, primarily to provide first, second, and third harmonic results for ease in analyses, but also to provide a compact means of data storage for subsequent use. These data have been completely tabulated in this data report. In each case a total of 10 harmonics are displayed for each unsteady channel.

Unsteady data for each pressure channel were reduced to dimensionless time history form by successive multiplications of the raw output (in computer counts) by the calibration constant for each channel (volt/count) and the calibration constant for each transducer (psi/volt); the results were then divided by the wind tunnel free stream dynamic pressure (psi) and by the blade pitching amplitude (rad). All results are harmonically referenced to the blade pitching motion (via Fourier analysis), and are normalized with respect to pitching amplitude.

Data Tabulations

All unsteady data, in reduced and normalized form, are contained in Tables 4 through 11. Mode 1 data are contained in this part of the data report in Tables 4 through 7, and Mode 2 data are contained in Part 2 of the data report in Tables 8 through 11. The sequence in each mode group is $\alpha = 2 \pm 0.5$ deg (Tables 4, 8), $\alpha = 2 \pm 2$ deg (Tables 5, 9), $\alpha = 6 \pm 0.5$ deg (Tables 6, 10), and $\alpha = 6 \pm 2$ deg (Tables 7, 10). Within each table are all combinations of interblade phase angle, α , and reduced frequency, k, for which data were taken, as listed at the beginning of each table. All notation used in these tables is fully defined in the list of symbols in terms of the original notation of Ref. 1. For each parameter pair (α and k), there are four pages of printout. These are different for each mode, and are described separately below.

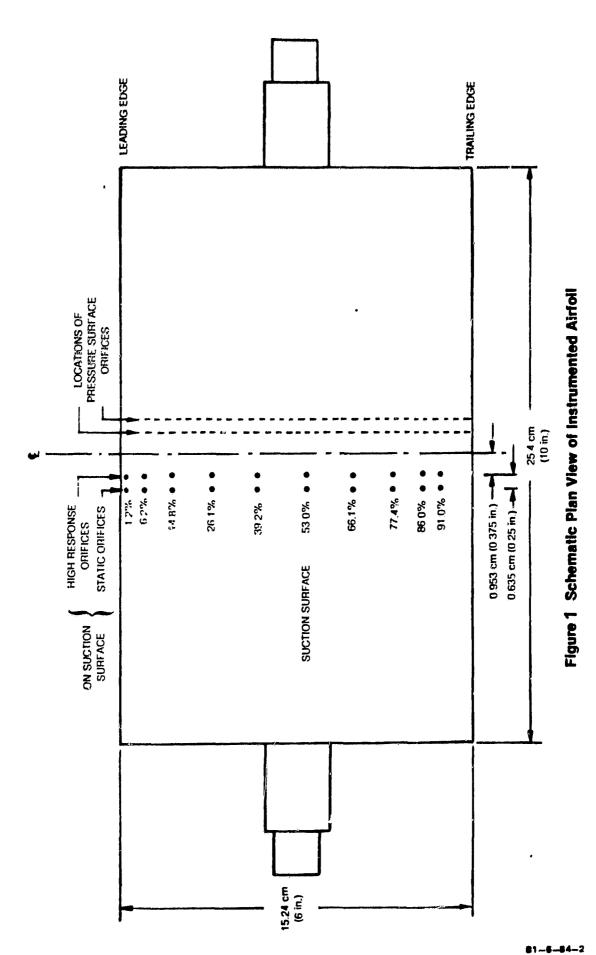
Mode I tables contain primarily center blade data with integrated loads and some sidewall data on the third and fourth pages. Pages 1 and 2 of each set have single surface pressure data for each chordwise location, with 10 harmonics listed vertically for each item printed (N is harmonic number). The first page lists real and imaginary parts and the second page lists amplitude and phase angle of these single surface results. Pages 3 and 4 of each set contain differential pressure results for all ten chordwise locations. In addition, there are lists of normal force coefficient, moment coefficient, the integrated aerodynamic damping parameter, and a group of single surface sidewall pressures. The third page has all harmonic lists in real and imaginary form while the fourth page presents these as amplitudes and phase angles.

Mode 2 tabulations are more graphical in that the data arrangement on each pair of pages is akin to the relative locations of the measurement stations in physical space. Pages 1 and 2 of each set contain real and imaginary parts and pages 3 and 4 of each set contain amplitudes and phase angles. For each pair of pages (arranged as facing pages in the tables, for convenience) blade number, and hence cascade location, is distributed lengthwise

on each page, while chordwise position on each blade is distributed crosswise on each page. (Note the isolated data for blade 4 at $\chi = .005$ and .030 on the suction surface, and the missing data for this blade at $\chi = .012$ on the pressure surface.) A single array of sidewall data is presented at the bottom of the tabulation on each pair of pages. To obtain the complete sidewall distribution for any desired combination of parameters, the reader should arrange the sidewall data from the appropriate pair of Mode 1, Mode 2 printouts in ascending order of gap fraction. (In such a case, it will be found that the run number is identical and the point numbers are consecutive.)

REFERENCE

1. Carta, F. O.: An Experimental Investigation of Gapwise Periodicity and Unsteady Aerodynamic Response in an Oscillating Cascade, Vol. I: Experimental and Theoretical Results. NASA CR 3513, 1982.



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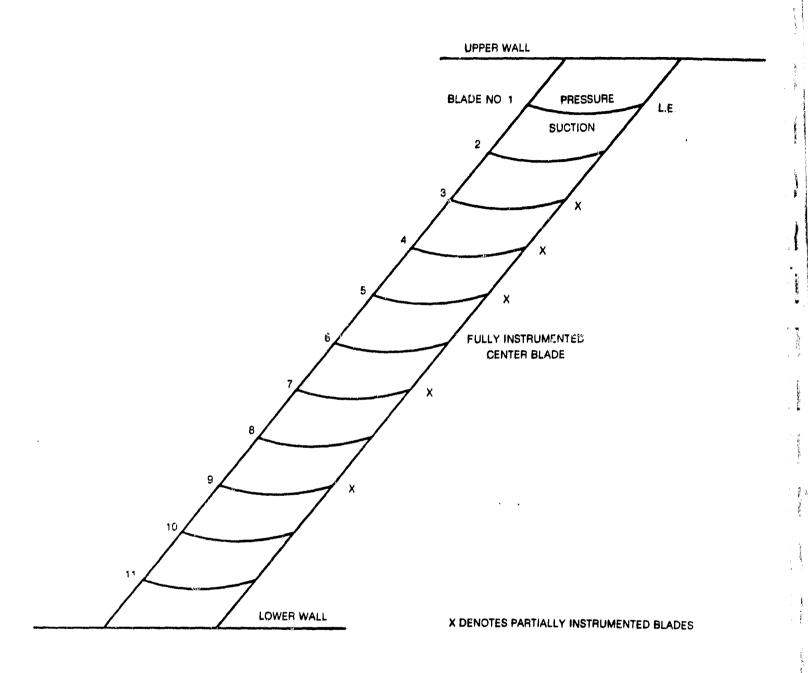


Figure 2 Schematic of Cascade Showing Instrumented Blades

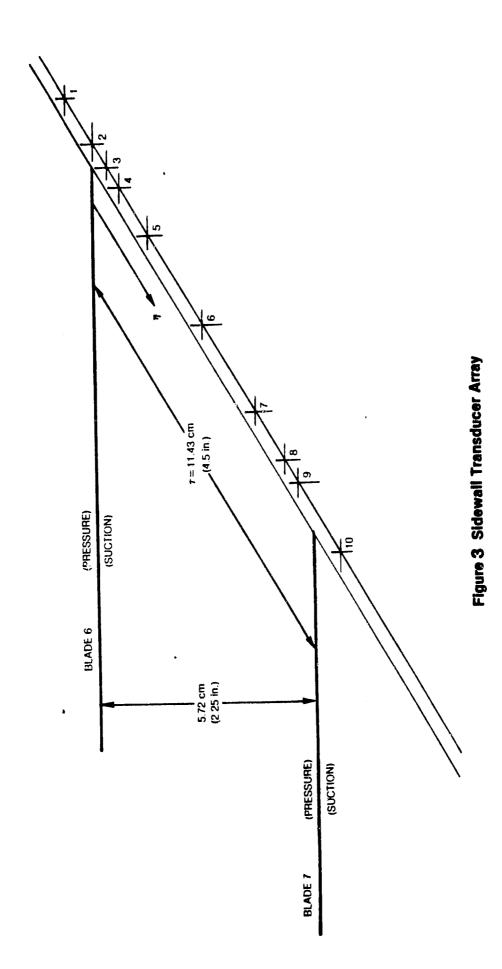


TABLE 1 DIMENSIONLESS AIRFOIL COORDINATES IN FRACTION OF CHORD c = 15.24 cm (6 in.)

RADIUS CENTER COORDINATES

	RADIUS CENTER COORDINATES
L. E. RADIUS/c = .0024	x = .0024, $y/c = .0002$
T. E. RADIUS/c = .0028	X = .9972, y/c = .0003

TABLE 2
TRANSDUCER ORIFICE LOCATIONS
(FRACTION OF CHORD)

a) Blade Transducers, Fractions of Chord

Blade	Values	of X
Number	Suction Surface	Pressure Surface
6	.0120	.0120
	.0622	.0622
	.1478	.1478
	.2612	.2612
	.3924	,3924
	.5297	.5297
i	.6608	.6608
	.7742	.7742
	.8598	.8598
	.9100	.9100
3,5,7,9	.0120	.0120
	.0622	
4	.0050	
	.0120	
	.0350	
	.0622	

b) Sidewall Transducers, Gap Fraction From Blade 6 Suction Surface

Wall Station Number	Gap Fraction n
1	125
2	.0
3	.062
4	.125
5	.25
6	.50
7	.75
8	.875
9	.938
10	1.125

TABLE 3
BLADE DATA CHANNELS

	MODE 1		MODE	2
ATLAS CHANNEL NUMBER	BLADE OR · WALL LOCATION	χ or η	BLADE OR WALL LOCATION	χ or η
1*		_	a	_
2*	a 6S1	.0120	6S1	.0120
2.* 3*	652	.0622	6S2	.0622
4	653	.1478	351	.0120
5	684	.2612	3S2	.0622
6	685	.3924	3P1	.0120
	6S6	.5297	451	.0050
7 8	657	.6608	4S2	.0120
9	6S8	.7742	453	.0350
10	659	.8598	484	.0622
10	6S10	.9100	581	.0120
12*	6P1	.0120	6P1	.0120
13**	6P2	.0622	582	.0622
14	6P3	.1478	5P1	.0120
15	6P4	.2612	751	.0120
16	6P5	.3924	782	.0622
17	6P6	.5297	7P1	.0120
18	6P7	.6608	951	.0120
19	6P8	.7742	952	.0622
20	6P9	.8598	9P1	.0120
21	6P10	.9100	w3	.062
21	W1	125 ·	w5	.250
22	W1 W2	.000	W7	.750
23 24 ³⁴	W2 W4	.125	W4	.125
	W4 W6	.500	w8	.875
25 26	W10	1.125	w9	.938

^{*} DENOTES REDUNDANT CHANNEL

NOTES: • Blade location notation ---

3S2 → blade 3, suction surface, second transducer aft of leading edge (P denotes pressure surface)

• Transducer location values ---

 χ is blade chord fraction η is sidewall gap fraction

MODE 1 DATA FOR $\alpha_{\text{MCL}} = 2 \text{ deg}$, $\overline{\alpha} = 0.5 \text{ deg}$

TABLE 4

σ (deg)	<u>k</u>	page
-135	.0714	18
11	.1230	22
11	.1523	26
-90	.0719	30
11	.1225	34
41	.1520	38
-45	.0715	42
ĬĬ	.1225	46
11	.1514	50
0	.0715	54
ĭi	.1210	58
11	.1503	62
45	.0722	66
ربه ۱۱	• •	
11	.1219	70
	. 1526	74
90	.0716	78
11	.1219	82
	.1507	86
135	.0717	90
11	.1227	94
11	.1526	98
180	.0714	102
11	.1213	106
†I	.1504	110

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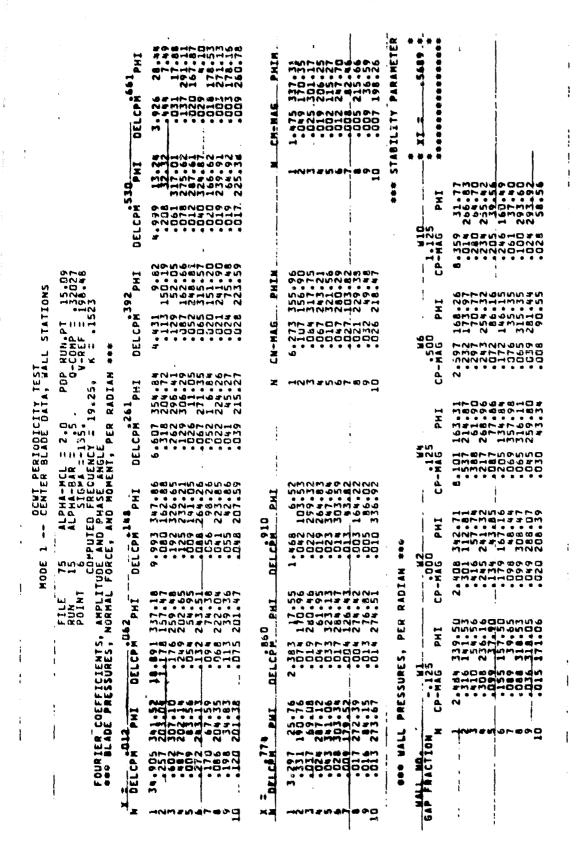
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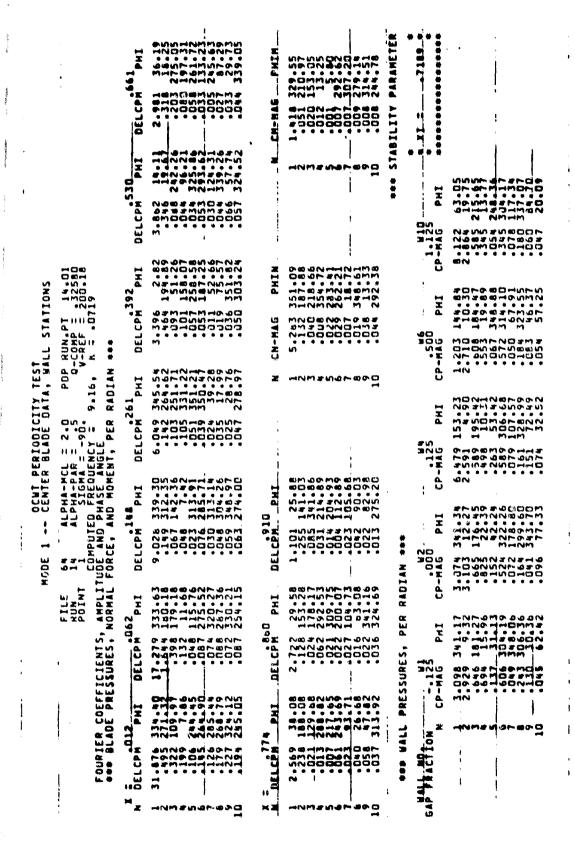
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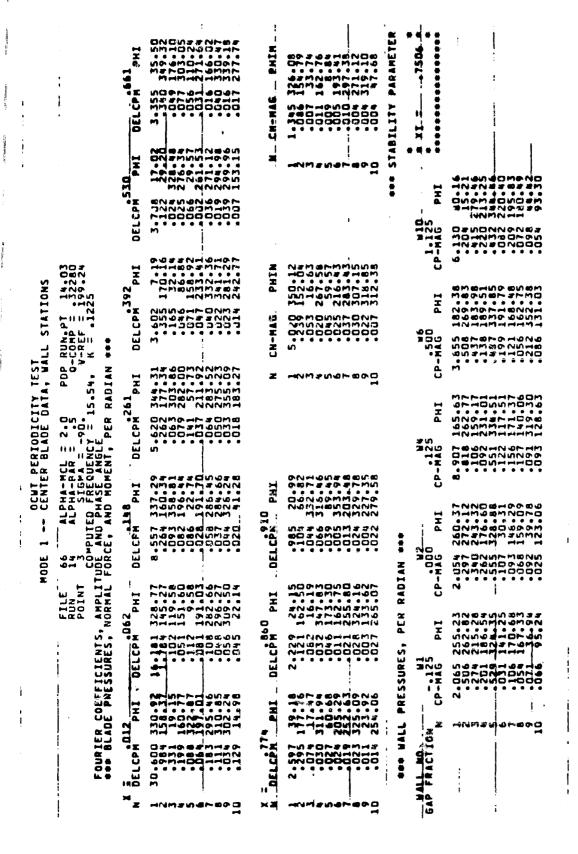


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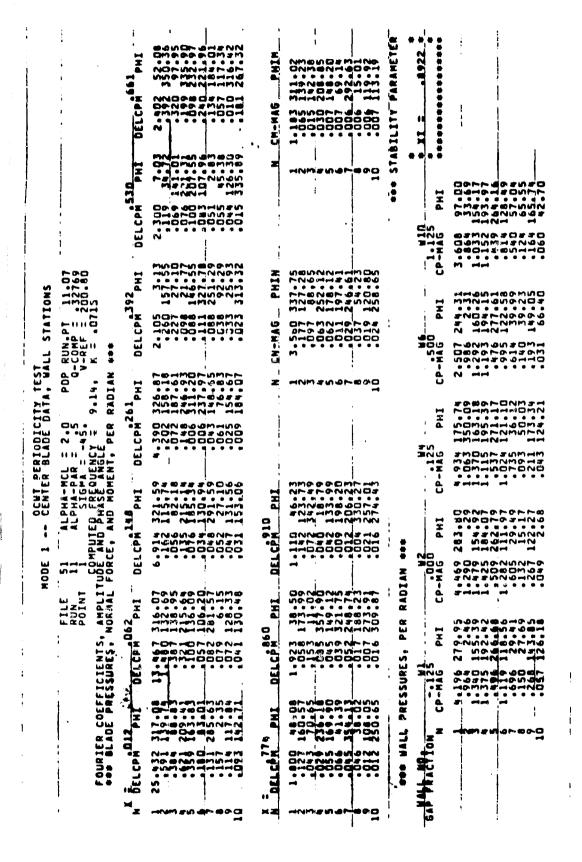
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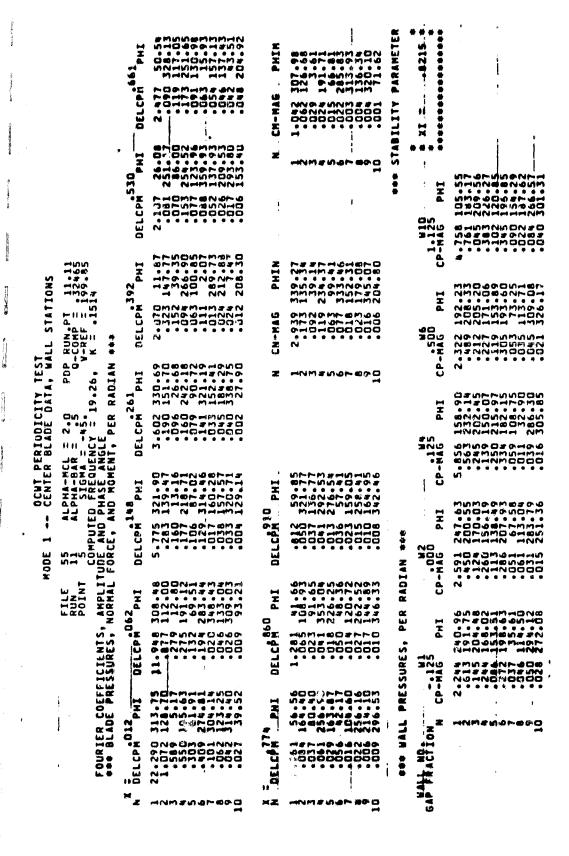
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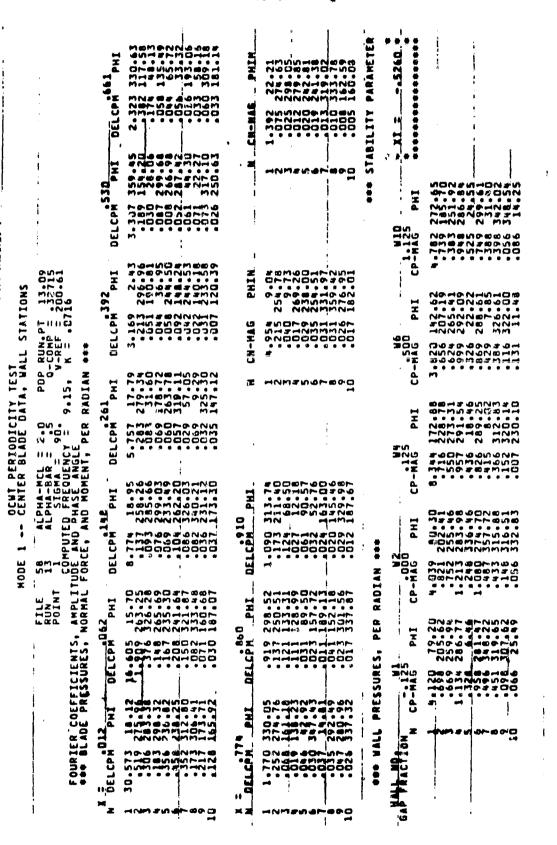
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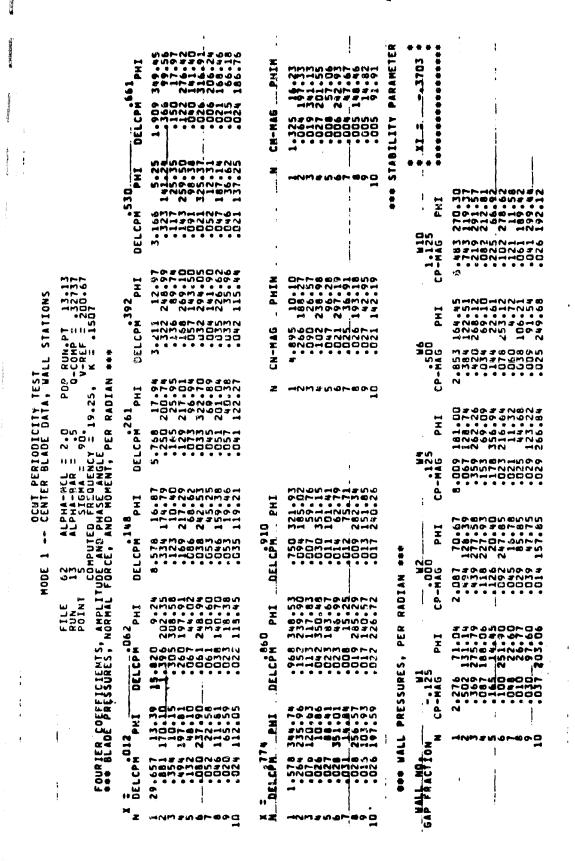
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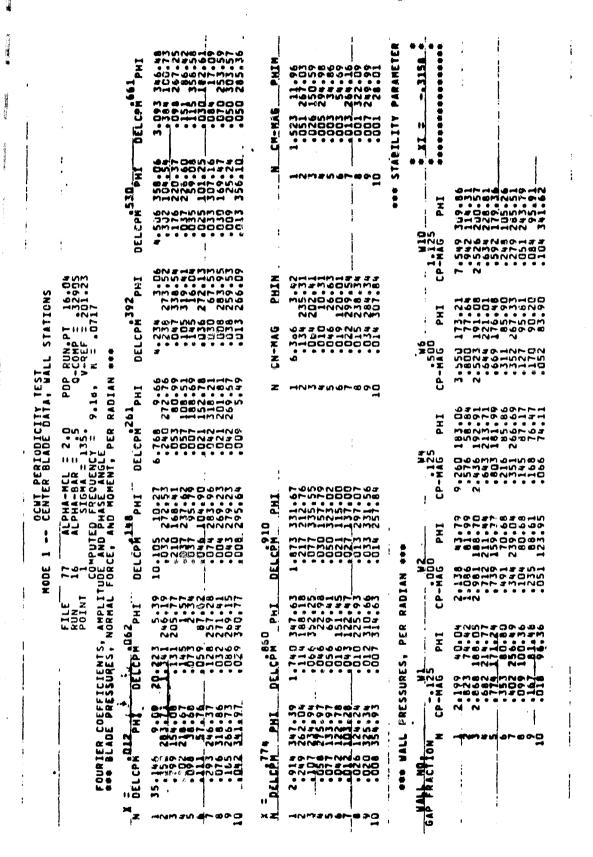
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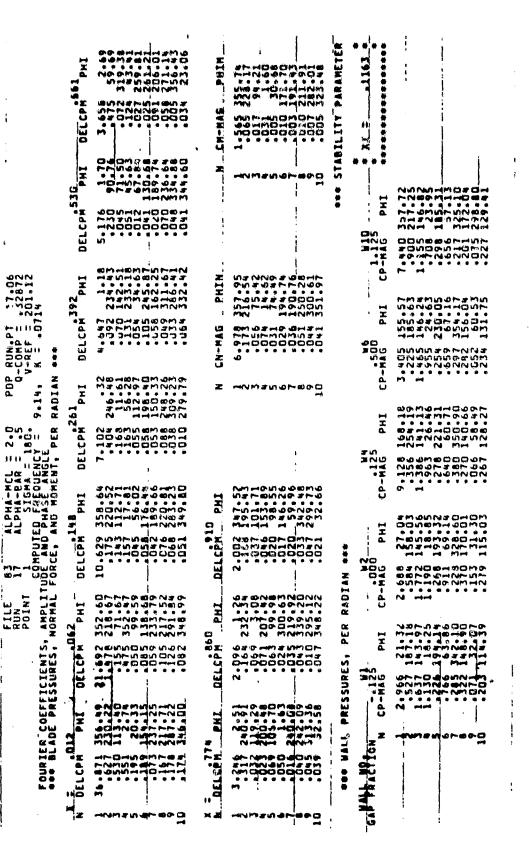
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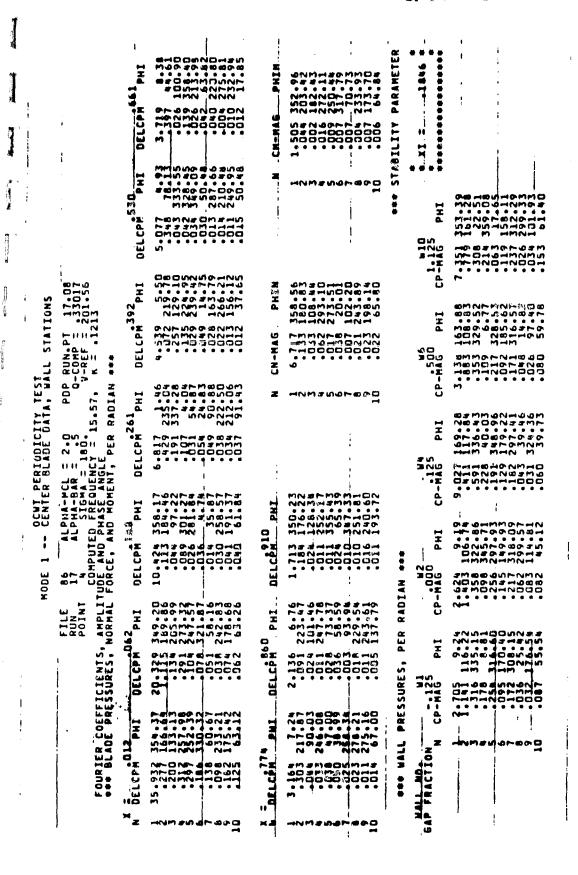
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TABLE 5

MODE 1 DATA FOR $\alpha_{MCL} = 2 \text{ deg}$, $\overline{\alpha} = 2 \text{ deg}$

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11	.1225	120
11	.1519	124
-90	.0722	128
11	.1218	132
11	.1504	136
-45	.0707	140
ii	.1214	144
11	.1508	148
0	.0724	152
11	.1228	156
11	.1491	160
45	.0724	164
11	.1223	168
f1	.1506	172
90	.0721	176
Ü	.1222	180
11	.1499	184
135	.0716	188
11	.1224	192
11	.1516	196
180	.0724	200
11	.1217	204
11	.1498	208

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MODE 1 CENTER BLADE DATA, WALL	FILE 3 ALPHA-MCL = 2.0 PDP RUN RUN 3 ALPHA-BAR = 2.0 0-COD SIGHT = 45. V-RE COMPUTED FRECUENCY = 15.54, N = FOURIER COEFFICIENTS, AMPLITUDE AND PHASE ANGLE *** BLADE PRESSURES, NORMAL FORCE, AND MOMENT, PER RADIAN ***	X SELCP# DELCP# DELCP# PHI DELCP# PHI DELCP# PHI D	36.964 26.02 12.907 23.77 7.265 28.83 %.694 30.21 2.442 134.26	= 1774 PHI _DELCPM PHI _ DELCPM PHI N GN	. 112 248.69 .109 236.09 .093 279.27 .1 3 .012 248.69 .109 236.09 .093 223.31 .2 248.69 .109 236.09 .009 237.57 .1 3 .002 37.03 .006 320.91 .006 237.57 .1 4 .002 37.03 .003 320.91 .006 25.69 .007 38.59 .011 35.84 .017 296.58 .007 38.59 .011 335.18 .012 20.59 14.65 .021 33.84 .10	*** WALL PRESSURES, PER RADIAN ***	P FRACTION125 P FRACTION125 N CP-MAG PHI CP-MAG PHI CP-MAG PHI CP-MA	
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OCHT PERIODICITY TEST -- CENTER BLADE DATA, WALL STATIONS

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		CP-KAG	20 40 40 60 60 60 60 60 60 60 60 60 60 60 60 60		CP-MAG	4 WWW - 400 4 WWW - 400 4 WWW - 400 4	2000	.910-1 CP-MAG	2450H	
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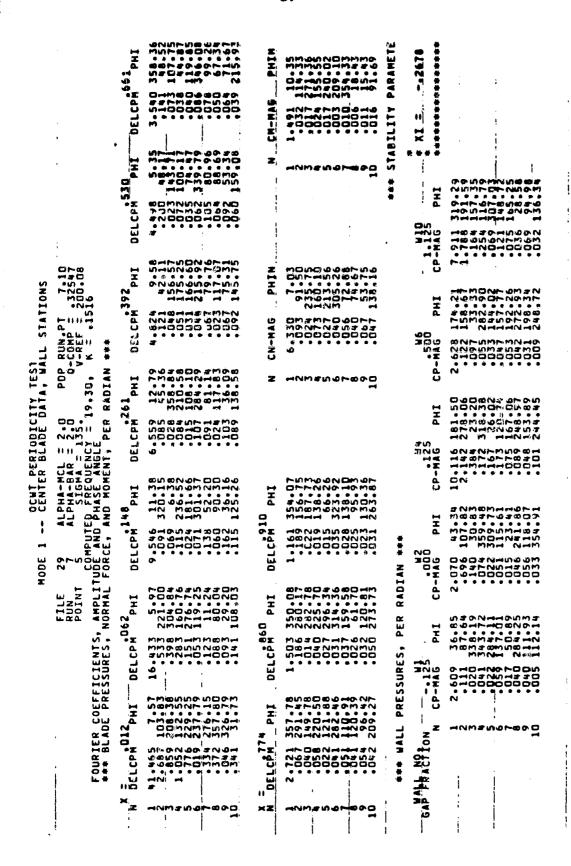
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TABLE 6

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11	.1196	242		
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11	.1230	254		
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45	.0718	262		
11	.1224	266		
11	.1507	270		
90				
90	.0714	274		
11	.1222	278		
	.1510	282		
135	.0726	286		
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TABLE 7

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11	.1493	368
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OCWI PERIODICITY TEST CENTEP BLADE DATA, WALL STATIONS

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	FILE 162 ALPHA-WCL = 6.0 PDP RUN.PT 32.0 6.0 ALPHA-E4R = 2.0 Q-COMP = 3255 POINT 1 SIGNA = 490. V-REF = 200.1 COMPIER COEFICIENTS, AMPLITUDE AND PHASE ANGLE 9.05, N = .0712.** BLADE PRESSURES, PER RADIAN ***	FILE 162 ALPHA-WCL = 6.0 PDP RUN.PT 32.01 50% 132.01 50% 2 3 ALPHA-WCL = 2.0 PDP RUN.PT 32.01 POINT 1 APPLITUDE AND PHASE ANGLE *** BLADE PRESSURES, PER RADIAN *** X = .G12-UPPER .062-UPPER .148-UPPER .261-UPPER .392-UPPER .6530-UPPER .661-UPPER .4651-UPPER .661-UPPER .4661-UPPER	FILE 162 ALPHA-WCL = 6.0 PDP RUN.PT 32.01 FOURIER COEFFICIENTS, AMPLITUDE AND PHASE ANGLE *** BLADE PRESSURES, PER RADIAN *** CD-MAG PHI CP-MAG PHI PHI CP-MAG PHI PHI CP-MAG PHI PHI CP-MAG PHI PHI CP-MAG PHI PHI CP-MAG PHI PHI CP-MAG PHI PHI CP-MAG PHI PHI CP-MAG PHI PHI CP-MAG PHI PHI CP-MAG PHI PHI CP-MAG PHI PHI CP-MAG PHI PHI PHI CP-MAG PHI PHI CP-MAG PHI PHI PHI PHI CP-MAG PHI PHI PHI PHI PHI PHI PHI PHI PHI PHI	FILE 162 ALPHA-WCL = 6.0 PDP_RUN.PT 32.01 FOURIER COEFFICIENTS, AMPLITUDE AND PHASE ANGLE *** BLADE PRESSURES, PER RADIAN *** *** BLADE PRESSURES, PER RADIA	FULE 162 ALPHA-CL = 6.0	x = CL12 - UPPER COEFFICIENTS, APPLITUDE AND PHASE ANGLE = -0.0 0 0 0 0 0 0 0 0 0

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		.530-UPPER CPREAL CPIMAG	-2.456 -1.345 -0040 -002 -0040 -0035 -000 -0035 -002 -006 -002 -006 -002 -006 -002 -006	.148-LOWER CPREAL CPIMAG	2.956 -1.911 -072 -008 -067 -008 -017 -035 -010 -610 -018 -005 -018 -008	.910-LOWER CPREAL CPIMAG	-108 -108 -108 -108 -101
LL STATIONS	UN.PT 32.03 .0MP = 32868 .aef = 201.08	*392-UPPEP CPREAL CPIMAG	-2.524 -786 -122 -174 -122 -174 -123 -023 -167 -024 -132 -1024 -132 -1024 -132 -1024 -132 -1024 -132 -1024	DOS-LOWER CPPEAL CPIMAG	# 5568 -2 927 - 1019 -	.860-LOWER CPREAL CPIMAG	- 1607 - 1613 -
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00 m	FILE 1 RUN POINT POINT ICTENTS, REAL E	SOFEST CPIPAG CPREAL CPIPAG	-6.322 2.196 -224 2.102 -001 0031 0054 -024 -004 0056 -004 0056 -004 0056 -0012	CPHEAL CPIMAG	-1.377 -1.257 -040 -052 -0640 -052 -069 -061 -050 -001 -050 -061	.53C-LOWER CPREAL CPIMAG	64000000000000000000000000000000000000
	FOURIER COEFF	• 012-UPPER REAL CPIMAG	1 -23.190 11.644 2 -33.190 11.664 4 - 629 3 4.16 5 - 162 4 - 019 6 - 163 3 - 247 7 - 163 - 012 8 - 165 - 012 9 - 165 - 103	X = .774-UPPER N CPPEAL CPIMAG	1 -1.72 -1.496 2657 -293 4654 -055 5607 -055 6 -017 -000 7 -021 -0067 8 -621 -067	X = .392-LOWER N CPREAL CPIMAG	2 - 993 - 701 2 - 912 - 283 4 - 655 - 6012 5 - 617 - 618 7 - 626 - 614 7 - 627 - 617 8 - 626 - 617 8 - 627 - 617 9 - 627 - 617 10 - 627 - 617 11 - 617

	.661-UPPER CP-MAG PHI	2.691 217-43 .274 179-23 .035 165-15 .013 165-15 .014 273-19 .019 354-10 .016 352-59 .016 352-59 .016 352-59	.261-LOWER CP-MAG PHI	2.260 326 .306 1813 .0065 1813 .018 313 .018 313 .018 313 .018 313 .018 131 .018 123 .0063 .0063		
	.530-UPPER CP-MAS PHI	2.8JD 208.71 .243 770.48 .046 173.70 .035 270.40 .025 346.65 .027 35.74 .027 35.74 .027 35.74 .027 35.74	.148-LOWER CP-MAG PHI	3.520 327.11 3.529 113.13 3.54 113.13 0.07 25.564 0.039 295.24 0.014 27.02 0.028 116.46 0.030 110.95	.910-LOWER CP-MAG PHI	.348 1085.97 .348 1085.97 .078 1085.02 .078 1085.02 .018 294.18 .018 284.18 .018 284.18
LL STATIONS RUN*PT 32.03 COMP = 32668 -REF = 201.06	CP-MAG PHI	2.644 197.27 .176 97.27 .066 64.43 .025 253.59 .019 346.48 .010 206.24 .011 37.08	.062-LOWER CP-MAG PHI	5.501 327 .589 148 .631 387 .631 386 .639 340 .628 2165 .626 2165 .626 17 .626 17 .637 283 .6137 283	. E60-LOWER CP-MAG PHI	235 197-25 276 104-652 2053 104-652 2053 267-25 2053 286-37 2017 17381 2017 3910-17
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00E 1 CENTER 164 ALPHA-PC 32 ALPHA-BA COMPUTED FREGU UDE AND PHASE A IAN ***	.148-UPPER CP-MAG PHI	3.992 169.31 .061 883.69 .131 883.69 .142 286.03 .042 286.03 .024 296.98 .024 296.98 .027 460.98	.910-UPPER CP-MAG PHI	1.578 219.35 .311 171.55 .633 176.28 .641 282.42 .017 330.57 .020 42.03 .020 33.93 .024 33.93	.661-LOWER CP-MAG PHI	209 322 56 144 18992 164 18992 1011 358 74 1018 298 74 1016 1718 1023 89 02 111 280 11
H FILE RUN POINT ICIENTS, AMPLITI SSURES, PLR RAD	CP-MAG PHI	6.692 led633 0.32 92.653 0.032 92.655 0.031 46.865 0.051 14.654 0.051 14.552 0.050 324.552 0.050 324.552	*860-JPPER CP-MAG PHI	1.864 222 39 040 177 10 062 37 86 012 282 39 017 323 11 017 14 91 023 14 91 012 323 50	.530-L0wER CP-MAG PHI	829 323 098 4 48 098 173 098 173 018 243 018 210 0046 25 005 125 005 1
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		DELCPM PHI	1.845 00.090 00.0000 00.000 00.000 00.000 00.000 00.000 00.000 00.000 00.000 00.0000 00.000 00.000 00.000 00.000 00.000 00.000 00.000 00.000 00.0000 00.000 00.000 00.000 00.000 00.000 00.000 00.000 00.000 00.0000 00.000 00.000 00.000 00.000 00.000 00.000 00.000 00.000 00.0000 00.000 00.000 00.000 00.000 00.000 00.000 00.000 00.000 00.0000 00.000 00.000 00.000 00.000 00.000 00.000 00.000 00.000 00.0000 00.000 00.000 00.000 00.000 00.000 00.000 00.000 00.000 00.0000 00.000 00.000 00.000 00.000 00.000 00.000 00.000 00.000 00.0000 00.000 00.000 00.000 00.000 00.000 00.000 00.000 00.000 00.0000 00.000 00.000 00.000 00.000 00.000 00.000 00.000 00.000 00.0000 00.000 00.000 00.000 00.000 00.000 00.000 00.000 00.000 00.0000 00.000 00.000 00.000 00.000 00.000 00.000 00.000 00.000 00.0000 00.000 00.000 00.000 00.000 00.000 00.000 00.000 00.000 00.0000 00.000 00.000 00.000 00.000 00.000 00.000 00.000 00.000 00.0000 00.000 00.000 00.000 00.000 00.000 00.000 00.000 00.000 00.0000 00.000 00.000 00.000 00.000 00.000 00.000 00.000 00.000 00.0000 00.000 00.000 00.000 00.000 00.000 00.000 00.000 00.000 00.0000 00.000 00.000 00.000 00.000 00.000 00.000 00.000 00.000 00.0000 00.000 00.000 00.000 00.000 00.000 00.000 00.000 00.000 00.0000 00.000 00.000 00.000 00.000 00.000 00.000 00.000 00.000 00.0	22	มือตลาดเกลเนนท	*** STA	#10 # 1.125 # -MAG PHI #	586 114.60 238 298 114.29 238 258 70 231 525.61 038 211.24 104 221.24 108 196.53 025 334.87
T ALL STATIONS	RUN.PT 29.03 -COMP = .32009 V-REF = 198.39 K = .0718	DELCPM PHI	2.154 354.36 .031 128.38 .035 1995.37 .023 278.82 .018 312.18 .025 51.63 .055 51.63	CN-MAG PHIN	3.241 .0528 1341 .0528 2228 .0528 2528 .0531 35528 .0558 1558 .0558 1558 .0558 1558 .0558 1558 .0558 1558 .0558 1558		#6 *500 -HAG PHI CP-	534 208 27 108 352 55 107 325 66 007 315 74 007 35 16 007 36 16 007 178 96 007 25 25
PERIODICITY TES R BLADE DATA, W	CL = 6.0 PDP AR = 2.0 0 UENCY = 9.07, ANGLE ENT, PER RADIAN	DELCP# 261 PHI	3.558 335.07 .103 688.38 .058 283.8 .058 287.986 .054 355.57 .059 350.55 .030 155.67	z	L0084694		.125 -MAG PHI CP	746 2159.79 1 746 216.69 1 367 1181.71 186 349.09 12.01 12.01 12.01 12.01 12.01 12.01 12.01 13.0
ODE 1 CENTE	144 ALPHA-M 29 ALPHA-P COMPUTED FIGH UDE AND PHASE FORCE, AND MOME	DELCP# PHI	5.80b 329.03 .163 79.92 .689 269.65 .689 269.65 .629 146.92 .629 110.13 .638 13.61 .638 13.61	DELCPM PHI	1.259 62.47 .009 174.04 .010 170.42 .008 352.72 .002 209.95 .003 229.95 .003 228.98	*** NA	W2 • 000 • AAG PHI CP	835 348.62 10 316 347.40 1 327 347.90 686 247.90 685 247.90 682 120.10 1095 120.10 1096 154.50 1006 261.84 024 60.45
Σ	FILE RUN POINT ICIENTS, AMPLIT SSURES, NORMAL	DELCPM PHI	9.613 326.84 .536 151.67 .129 243.97 .1129 243.97 .019 44.30 .011 154.40 .021 151.42 .060 21.63	DELCPM PHI	882 77.74 0042 233.17 0042 242.35 0012 242.64 0010 280.85 000 280.80 000 280.80 000 280.80 000 280.80	SURES, PER RADI	• 125 MAG	858 285.34 331 51.78 100 291.48 091 60.36 106 26.23 075 168.47 016 246.70
	FOURIER COEFF *** BLADE PRE	X = .012 N DELCPM PHI	1 31.47U 324.14 2 2.993 164.07 3 2.086 23.390 4 26 158.65 6 426 158.65 7 151 13U.27 8 328 328.50 9 229 159.25 16 055 293.39	X = DELCPH PHI	1 1.348 59.79 2 077 306.46 3 023 346.25 4 001 235.18 5 0004 42.78 6 0001 42.78 7 0003 142.88 8 0003 143.58 9 0003 146.63	*** WALL PRES	WALL NO.	100 84 MN 100 100 100 100 100 100 100 100 100 10

		.661-UPPER CPREAL CPIMAG	.332 -1.725 .363 -0.64 .002 -0.64 .003 -0.028 .007 -0.09 .003 -0.09	.261-LOWER CPREAL CPIMAG	19431 -1.575 314 -224 0002 -020 0039 -022 0011 -013 0010 -033 0011 -014		
		-UPPER CPIMAG	11. 10.00000000000000000000000000000000	LOWER	-2.278 -2.278 -2.228 -2	LOWER	
		CPREAL		CPREAL	2	.91J-	
TIONS	229 3221 198 198 199	UPPER CPIMAG	######################################	CPIMAG	-3.20 3.359 -1.0013 -1.0007 -1.0007	OWER CPIWAG	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
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		UPPER CPIMAG	######################################	CPIMAC	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	OWER CPIMAG	10000000000000000000000000000000000000
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	UPPER PHI	153 233 33 33 33 33 33 33 33 33 33 33 33 3	UPPER PHI	247 247 2541.27 2541.27 10065.26 10065.27 10065.27 10065.27	OWER	319 319 3182 3182 3182 3182 3184 32 32 46 31 46 31 46 31 46 31
A** NA	.146- CP-MAG	N	. 910-U	1.22 2.22 2.22 2.22 2.22 2.22 2.22 2.22	. 661-L CP-MAG	
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SSURES,	-062- CP-MAG	4	.860-U CP-MAG	1 22 23 23 23 23 23 23 23 23 23 23 23 23	. 530-L	1 000000000000000000000000000000000000
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*** BL	= .012- CP-MA6	2 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	CP-MAG	1. 6.52 6.00 6.00 6.00 6.00 6.00 6.00 6.00 6.0	CP-MA6	60000000000000000000000000000000000000
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STATION - PI - 3 - 19 - 1 - 1 - 1 - 1 - 2 - 1 - 2 - 1 - 2 - 1 - 2 - 1 - 2 - 2	392 LCPR DE	2404M04C000	EAL CA	490000000 49000000000000000000000000000		6 CPIMA	**************************************
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	SELCPM PHI	11.66.9 11.00.9 10.			S ***	M10 125 AG PHI	144 110.33 14 65.67 34 34 2-10 34 34 2-11 153-18 152-18 152 22-6 18 22-6 18 22-6 18 22-6 18 22-6 18 22-6
IONS 29.05 32136 198.79	.392 PHI D	25.00	PHIN	2133 21198 20198 2		HI CP-H	25.00.00.00.00.00.00.00.00.00.00.00.00.00
EST WALL STAT DP RUN.PT 0-COMP = V-REF = N = 12	I DELCPÅ	1. 95 5. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	N CN-MAG	22 23 24 24 25 26 26 26 26 26 26 26 26 26 26 26 26 26		#6 *50C CP-MAG P	1.183 200 0.0472 2447 0.0472 2447 0.049 2407 0.019 2883 0.029 2883 0.029 2883
ILUDICITY T ILADE DATA, = 6.0 P = 2.0 -45.0 -45.0 -15.46 ICY = 15.46 ICY = 15.46	*261	3.212 333 0059 332 0037 176 035 951 030 287 0015 268 0019 224		Print.		25 16 PHI	1153 1153 1153 1153 1153 125 125 125 125 125 125 125 125 125 125
- CENTER BRALPHA-WCL	148 PHI D	324.56 355.888 245.746 1211.51 1611.50 248.25 232.85 197.02 197.03 197.03	10 PHI	55.882 2.994 2.895 2.860 2.895 2.994 3.994 3.996 3.996 1.956		HI CP-MA	11 100.000 100
HODE 1 - 146 17 29 17 CGMPUT ITUDE AND	UELCP#	5	T DELCPH	1.000 000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.	10 I AN ***	. ×	1,914 351 1,914 351 1,914 351 1,913 275 1,014 254 1,017 289 1,017 289 1,017 289
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RIER COEFFI BLADE PRES	*012 CP# PHI	308 317 587 262.56 148 26.56 148 26.94 364 131.35 271 339.88 150 252.74 108 252.74	.774 PHI	427 61.23 127 302.05 024 304.96 012 348.93 017 294.12 010 157.43 002 269.09 006 216.55	* WALL PRESSI	N CP - S	42224200000000000000000000000000000000
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ERIODICIT BLADE DA	F = 6*0 = 2*0 = -45* ENCY = 1	CPREAL	-2.071 -021 -023 -022 -0022 -0014 -0008	CPREAL	**************************************	.774-L CPREAL	00000000000000000000000000000000000000
OCUT PE CENTER	LPHA-MC LPHA-MA SIGWA D FPECU	UPPER CPIMAG	00000000000000000000000000000000000000	PPER CPIMAG	1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-	OWER CPIMAG	10004 00004 00004 00000 00000
0DE 1	148 A S S S S S S S S S S S S S S S S S S	CPDEAL	-2.921 -0.38 -0.011 -0.009 -0.009 -0.000	CPEEAL	000000000000000000000000000000000000000	.661-L CPPEAL	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
x	FILE RUN POINT REAL E	UPPER CPIMAG	2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	PPER CPIMAG	-1- -0.004 -0.003 -0.003 -0.005 -0.00	OWER CPIMAG	000000000000000000000000000000000000000
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	R COEFF	UPPER CPIMAG	15.232 -4112 -4112 -1123 -1110 -1110 -1110	PPER CPIMAG	-1.0684 -1.0084 -1.0017 -1.0017 -1.0017 -1.0017	OWER CPIMAG	00000000000000000000000000000000000000
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		4.4	N	CP-126	- · · · · · · · · · · · · · · · · · · ·		
		-UPPER PHI	23244 2326 2326 2326 2326 2326 2326 2326	LOWER	2009 2009 32009 2009 2009 2019 2019 2019 2019 2019	LOWER	2433-44 2433-44 2433-62 2433-6
		CP-14 AG	2	CP-MAG	24 24 24 24 24 24 24 24 24 24 24 24 24 2	.91J-E	**************************************
IGNS	29.07 32013 98.40	UPPER PHI	2006.94 2344.27 2344.27 2366.14 2066.14 2866.68 2866.68 2966.11	OWER	2008-27 3008-27 3008-27 1721-46 3174-43 283-153 283-156 283-156 283-156	OWER	22916. 22916. 22418. 3301652 3011652 2045. 2045. 2045. 2045.
LL STAT]	COMP TAREF TAREF TAREF TAREF	.392- CP-MAG		CP-MAG	W	1-398. CP-846	
TY TEST ATA, WA	P.0 0.0	UPPER PHI	25.50 25.50 25.00 25.40 25.40 176.25 176.25 25.00 27 25.00 27 25.00 27 25.00 27 25.00 27 25.00 27 25.00 27 25 26 37 25 37 25 37 37 37 37 37 37 37 37 37 37 37 37 37	OWER PHI	309.55 1899.65 171.34 171.34 310.32 310.32 308.10 97.36	OWER PHI	2833.69 2884.43 2823.46 3892.988 3223.65 552.65 146.14
ERIODICI BLADE D	R = 2.0 = 2.0 = -45. ENCY = 1 NGLE	CP-MAG	2.0102000000000000000000000000000000000	CP-MAG	60000000000000000000000000000000000000	.774-L CP-HA5	######################################
CENTEP	LPHA-VC LPHA-PA SICVA FRECU PHASE A	JPPER PHI	2254 2256 2356 2357 2357 2557 2557 2558 2573 2573 2573 2573 2573 2573 2573 2573	PPER PHI	224 224 236,53 2036,32 2036,32 2036,32 2036,32 2036,32 2036,32 2036,33	OWER PHI	2556.58 274.004 321.6.004 321.6.004 321.6.004 256.23 180.21 160.22
00E 1	146 A 25 CC-FUTE UDE ANJ	*146- CP-PA6	3 1000000000000000000000000000000000000	610-U		. 661-L CP-HAG	
š	FILT RUN POINT AMPLITE	UPPER PHI	MANAMANAN MANAMAN MANA	PPEK PHI	22 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	O BER PHI	22629 22629 326922 326922 125528 125528 125538 1255
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ERIJDICITY TEST BLADE DATA, WA	R = 2.0 0- ENCY = 15.44, NGL. NY, PER RADIAN	DELCPM PHI	2.267 .095 291.41 .024 326.63 .012 327.56 .016 52.50 .014 100.41 .034 3310.25 .004 115.26	z	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		.125 MAC PHI CP-	857 175.72 1.6592 253.69 655 128.84 6149 30.74 10.00 1
ODE 1 CENTER	14C ALPHA-BA 28 ALPHA-BA SIGWA CGPPUTED FRECU UDE AND PHASE AN	DELCPM PHI	3.5597 3588.73 3.6573 3388.73 3.012 3485.156 5.013 3485.156 5.013 1907.83 5.012 3107.83 5.012 183.83 5.017 183.83	DELCPM PHI	. 556 126.96 . C12 236.96 . C12 236.93 . C07 66.37 . C09 328.20 . C07 288.20 . C01 226.35 . C01 226.35	***		23 358.64 787 285.64 154 285.64 155 289.92 556 155.95 607 28.63 144 168.15 018 17.43
ř	FILE HUN POINT ICIENTS, AMPLIT SSURES, NGAMAL	DELCPM PHI	5.8867 355.61 189 269.36 104 9 9156 1018 265.82 1032 155.19 1026 274.79 1013 143.75 1013 143.75	DELCPM PHI		SURES. PER RADI	#1 #125 MAG PAI CP-	2397 157 256 27
	FOURIER COEFF *** BLADE PRE	X = .012 N DELCPM PHI	1 22.231 351.26 3 2551 283.40 3 6551 283.40 4 6588 246.53 6 641 197.50 7 14.50 7 14.50 7 14.50 7 14.50 7 15.50 10.02 171.57	X = DELCPM PHI	1 .658 124.97 3 .042 25.06 4 .018 23.20 6 .013 354.18 6 .013 354.18 7 .013 294.59 7 .019 352.58 9 .019 245.62	*** WALL PRES	ON CP	

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		-UPPER PHI	335.54 106.659 2106.559 106.559 187.651 18.20 18.20 24.663	LOWER	11 12 19 19 19 19 19 19 19 19 19 19 19 19 19	LOWER	212223 212323 222323 22333 22333 22333 233 2333 2333 2333 2333 2333 2333 2333 2333 2333 2333 2333 2333 233 2333 2333 2333 2333 2333 2333 2333 2333 2333 2333 2333 2333 233 2333 2333 2333 2333 2333 2333 2333 2333 2333 2333 2333 2333 233 2333 2333 2333 2333 2333 2333 2333 2333 2333 2333 2333 2333 233 2333 2333 2333 2333 2333 2333 2333 2333 2333 2333 2333 2333 233 2333 2333 2333 2333 2333 2333 2333 2333 2333 2333 2333 2333 233 2333 2333 2333 2333 2333 2333 2333 2333 2333 2333 2333 2333 233 2333 2333 2333 2333 2333 2333 2333 2333 2333 2333 2333 2333 233 2333 2333 2333 2333 2333 2333 2333 2333 2333 2333 2333 2333 233 2333 2333 2333 2333 2333 2333 2333 2333 2333 2333 2333 2333 233 2333 2333 2333 2333 2333 2333 2333 2333 2333 2333 2333 2333 233 2333 2333 2333 2333 2333 2333 2333 2333 2333 2333 2333 2333 233
		.530-CP-MAS	######################################	CP-4AG		913-1	1.00.00.00.00.00.00.00.00.00.00.00.00.00
IONS	28.08 32292 199.28 01	-UPPFR PHI	223.73 223.73 106.85 2558.10 2473.65 34.41 286.30	LOWER	3074 11173 1173 1190 1166 1166 1156 1156 1156 1156 1156 115	OWER	46.33 1116.33 1254.03 254.05 270.43 152.96 42
LL STATE	KUN. PT COMP I -REF I	392. CP-H&G		.062-I	2.711 .00899999999999999999999999999999999999	CP-MAG	7.300.000.00 200.000.00 200.000.00
ITY TEST DATA, WA	PDP 0- 19-04,	-UPPER PHI	1102-75 1102-75 1102-75 2455-40 25-40 23-67 342-52 342-53 342-338	LOWER	0.3110000000000000000000000000000000000	LOWER	233.657 234.698 234.698 234.698 234.694 224.944 1123.004
ERIODIC BLADE	1	CP-MAG	**************************************	.012-	4 ••••••••••••••••••••••••••••••••••••	-774- CP-HAG	1.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
- CENTER	ALPHA+PA ALPHA+PA SIGMA ED FREGU PHASE A	-UPPER PHI	117266. 117266. 12726. 12726. 12736. 14536. 14536. 16136. 17	UPPER PHI	9.76 20.569 11145.699 1100.133 1100.133 1100.133 1100.133 1100.133 1100.133	LOWER	22468844 22246884 22246884 561498 56149 56149 561498 56149 56149 56149 56149 56149 56149 56149 56149 56149 56149 56149 56149 561
100E 1 -	142 28 CGMPUT UDE AND	CP-MAG	1. ************************************	. 910-		. 661-1 CP-HAG	1.054 2603 2603 2603 2603 2603 2603 2603 2603
3.	FILE HUN POINT	-UPPER PHI	173.22 22.24.152 10.08.10.0 26.78.10.0 6.24.47 20.1.26 20.25 20.25 20.25 20.25	JPPER PHI	1004 1004 1004 1004 1004 1004 1004 1004	OWER PHI	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
	TCLENTS	CP-MAG	3. 6026 6026 6000 6000 6000 6000 6000 600	CP-48G	11	.530-L CP-MAG	1.20 0.00 0.00 0.00 0.00 0.00 0.00 0.00
	ER COEFF LADE PRE	-UPPER PHI	1171 10091 15091 10091 1	UPPER PHI	359 1116 1116 1232 1023 1023 146 146 166 166 166 166 166 166 166 166	LOWER	29.16 21.17.27 22.0.27 22.0.27 22.0.37 22.0.37 22.0.37 21.0.17 11.0.17
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		DELCPH PHI		H-HAG PHIM		LITY PARAMETER	**************************************										
		DELCPM PHI	1.154 60.65 .061 304.87 .013 2515.42 .015 40.33 .019 244.21 .017 221.42 .017 221.42	Z Z	๚๛๛๚๛๛๛๛๚	*** STARI	#10 * X *125 * * X MAG PHI ***	207 144.44 095 224.39 049 1214.17 049 151.30 085 151.56 015 168.28 011 157.93 010 13.48									
IT STATIONS	AUN.PT 28.05 1-COMP = 32292 V-REF = 199.28 K = .1501	DELCPH PHI	1.443 1.136 287.110 1.19 2.64.33 1.19 2.14.39 1.10 2.14.39 1.10 1.12.89 1.10 1.12.89 1.12.89	CN-MAG PHIN	1.995 13.57 1.01 300.57 1.01 310.56 1.02 228.93 1.01 218.93 1.01 21 21 1.01 203 1.01 203 1.01 203 1.01 203 1.01 203 1.01 203 1.01 203 1.01 303 1.01 303		.500 -500 -MAG PHI CP-	417 204 85 163 90 48 659 201 62 007 132 95 007	PERIUDICITY TES	AAR = 2.0 PDP AAR = 2.0 OUENCY = 19.04, ANGLE ENT, PER RADIAN	DELCP# PHI	2.362 134 29981 1034 29981 1034 2193 1014 2193 1018 2265 1018 226 1018 1145 1018 1145 1145 116 116 116	Z			N4 125 -#A6 PHI CP	. 206 177-23 -677 256-38 -679 266-38 -038 56-08 -032 33-97 -032 33-97 -035 74-55 -011 212-65 -021 74-80
PODE 1 CENTE	142 ALPHA-P 28 ALPHA-R 106 AD SIGN TUDE AND PHASE FORCE, AND MOM	.148 O£LCPM PHI	3.775 115 316 15 105 3 16 16 103 3 19 16 103 19 16 103 17 16 103 18 19 103 17 18	DELCPH PHI		### NVI	• 10	.426 358.64 8 .318 2811.34 .103 2844.76 .011 175.90 .010 354.887 .006 351.58									
	FILE HUN FUNT POINT POINT FICIENTS, AMPLI	OELCPP PHI	6.14 # 357.8 # # 357.8 # # 022	DELCPM PHI	685 142.23 037 925.43 0012 3255.43 0013 1595.73 0012 240.11 0010 171.95 009 226.55	SSURES, PER RAD	#1 *125 MAG PHI CP	164 E4 80 0026 1026 1026 1026 1026 1026 1026 102									
	FOURIER COEF	X = .012 N DELCPM PHI	1 22.737 351.84 2 .676 263.09 3 .524 525.37 4 .523 225.37 6 .084 287.16 6 .189 179.52 7 .065 169 8 .042 97.91 10 .052 88.25	X = 0ELCPH PHI	1 .888 115.11 3 .054 21.42 4 .015 252.12 5 .010 78.18 6 .021 251.95 7 .012 251.95 7 .015 259.11 9 .015 235.73	*** WALL PRE	Z Z	- Company									

		UPPER	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	ONER	6-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1		
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LL STATI	COMP T COMP T PEF T K T G G Z	CPREAL		.062-1 CPREAL	2 1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	CPREAL	11
ITY TEST DATA, WA	PDP 0-0 9.05,	UPPER CPIMAG	00000000000000000000000000000000000000	LOWER	3.171 	LOWER CPIMAG	50000000000000000000000000000000000000
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- CENTER	ALPHA-MC ALPHA-RA SIGNA ED FRECU	UPPER Colvag		UPPER CPINES		CPIMAG	
ODE 1	150 Å 150 A 100MPUTE 1MAGINA IAN ***	.148-	-3.283 11253 1221 6212 621 631 631 631	.910-L	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	.661-1 CPREAL	
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	R COEFF ADE PPE	-UPPER CPIMAG	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	JPPER CPIMAG	00000000000000000000000000000000000000	LOWER CPIMAG	
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		CP-HAG		CP-MAG	######################################		
		UPPER	50 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	OWER	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	OWER	2055-11 2055-11 2056-21 2056-21 2056-21 2056-22 2056-42 2056-42 2056-42
		CP-4A6	1	.148-L	2,748 0.000 0.000 0.000 0.000 0.000 0.000	.913-L	000000000000000000000000000000000000000
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OCWI PERIUDICITY TEST -- CENTER BLADE DATA, WALL STATIONS

•		PI DELCPR DELCPI	188	N CHREAL CHIMAG	1 1.015 2 037 4 0013 4 0002 6 0009 7 0002 6 0002 7 0002 8 0002 9 0002 10 0003 10 0003	STABILITY PARAMETER	# XI = +,4757 # # # # XI = + # # XI = + # # # # # # # # # # # # # # # # # #	,
		DELCPR DELC	1.566 		•	S ***	MID 1.125 PEAL CPIMAG	
TATIONS	PT 30.01 = 32578 = 203.16 .0710	.cps DELCPI	1176 - 671 1067 - 107 1052 - 0055 1013 - 0049 1003 - 0015 1003 - 0015 1004 - 0025	AL CNIMAG	130 1.015 053 .083 0017 .006 017 .009 017 .004 0017 .004 0016 .004		G CPIMAG CP	00000000000000000000000000000000000000
ITY TEST DATA: WALL S	PDP RUN. 0-COMP V-REF 9.05, K = RADIAN ***	261 DELCPI DEL	1.5443 0.0058 0.0058 0.0058 0.0056 0.0056	N CNRE	4084066893		#6 SOT MAG CPREAL	-1.676 012 349 349 177 059 059 065 065 065 065 065 065 065 065 065 065
WT PERIODIC	A-PAP = 2.0 IGFA = 45. REQUENCY = MOMENT, PEP	CPI DELCPR	401 114 2023 0031 0031 0031 0032 0032 0033 0042 0042 0043 0044 0044	CPI	0406 0001 0000 0000 0000 0000 0000		W4 125 CPPEAL CPI	-11.122 -2. 414 -1. 293 115 114 144 144 144
100E 1 CE	150 ALPH 10 ALPH 1 ALPH 1 ALPH S COMPUTED F IMAGINARY FORCE, AND	DELCPR DEL	5 492 2 2 124 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	DELCPR DEL	000000000000000000000000000000000000000	*** 24	B G C C	74661 7467 7467 747 747 747 747 747 747 747 7
Σ	FILE RUN POINT IENTS, REAL E URES, NORMAL	ELCP® DELCPI	9.002 3.617 -134 006 -053 -017 -014 -003 -016 -003 -019 -003	ELCPP DELCPI		0.00	T CPIMAG CP	23.3.3.4.4.6.6.6.6.6.6.6.6.6.6.6.6.6.6.6.
	OUPIER COEFFIC	LCP& DELCPI D	314 11.661 685 - 1.661 2094 - 2.393 6125 - 1.15 6420 - 2.77 664 - 1.66 665 - 1.66 665 - 1.66 665 - 1.66 665 - 1.66 665 - 1.66	LCPR DELCPI D		I DO S G G I I W T T T T T T T T T T T T T T T T T	NO. ACTION CPRE	HVW-PO OCOUNT
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		DELCPM	######################################	CH-MAG	M 24 M M4	ILITY P	= IX	
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Y TES	PCP 0 .05, ADIAN	1 PHI	2007-100 30000000000000000000000000000000000	z	H0w2204		3	HOWENBOBBN
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	FILE 156 ALPHA-MCL = 6.0 PDP RUN.PT 31.0 RUN 31 ALPHA-PAR = 2.0 9-COMP = 3239 POINT 1 SIGMA = 90. V-REF = 199.6 COMPUTER COEFICIENTS, REAL E IMAGINARY ** BLADE PRESSURES, PER RADIAN ***	FILE 156 ALPHA-MCL = 6.0 PDP RUN.PT 31.04 FUN 31 ALPHA-PAR = 2.0 9-COMP = 32399 POINT 31 ALPHA-PAR = 2.0 9-COMP = 32399 COMPUTED FREGUENCY = 9.11, K = .0717 *** BLADE PRESSURES, PER RADIAN *** X = .012-UPPER .062-UPPER .392-UPPER .530-UPPER .661-UPPER CPREAL CPIMA	FILE 156 ALPHA-MCL = 6.0 PDP RUN.PT 31.04 FOURIER COFFFICIENTS, REAL E IMAGINARY *** BLADE PRESSURES; PER RADIAN *** **	FILE 156 ALPHA-PCL = 6.0 90P RUN.PT 31.04 FOURIER COFFICIENTS, REAL E INAGINARY X = 012-UPPER N C CAPUTED FRECUENCY = 9.11, K = .0717 C CAPUTED FRECUENCY = 9.11, K = .0717 C CAPUTED FRECUENCY = 9.11, K = .0717 X = 012-UPPER N C CAPUTED FRECUENCY = 9.11, K = .0717 S = 012-UPPER N C CAPUTED FRECUENCY = 9.11, K = .0717 X = 012-UPPER N C CAPUTED FRECUENCY = 9.11, K = .0717 S = 012-UPPER N C CAPUTED FRECUENCY = 9.117 S = 012-UPPER N C CAPUTED FRECUENCY = 9.117 S = 012-UPPER N C CAPUTED FRECUENCY = 9.117 S = 012-UPPER N C CAPUTED FRECUENCY = 9.117 S = 012-UPPER N C CAPUTED FRECUENCY = 9.117 S = 012-UPPER N C CAPUTED FRECUENCY = 9.117 S = 012-UPPER N C CAPUTED FRECUENCY = 9.117 S = 012-UPPER N C CAPUTED FRECUENCY = 9.117 S = 01	FOURTER COEFFICIENTS, PRAIL LIST ALPHA-PCL = 6.0 POP RUN, PT 31,339 PO	FOURTHER COEFFICIENTS FILE 15

	.661-UPPER CP-MAG PHI	1.617 129.18 .454 35.611 .365 25.99 .041 42.99 .131 250.40 .035 255.71 .013 263.21	.261-LGWEP CP-MAG PHI	2.602 .323.357.221 .034.357.221 .036.258.47 .030.251.83 .044.221 .030.253.44 .024.100.28 .068.253.47 .014.253.47		
	.530-UPPER CP-MAS PHI	1.834 142.28 .446 140.24 .548 48.28 .049 41.44 .032 259.65 .032 259.53 .032 259.53	.143-LOWER CP-MAG PHI	3.88.9 3.10 3.27.67 0.85.9 10.	.91J-LOWER CP-MAG PHI	.211 119.29 .358 25.10 .358 25.10 .014 25.00 .011 245.00 .011 245.00 .011 245.00 .011 245.00 .011 259.00
LL STATIONS RUN.PT 31.04 COMP = 32399 -FEF = 199.62 K = .0717	CP-HAG PHI	1.742 159.07 .277 22.15 .077 62.15 .059 46.68 .140 249.27 .168 110.825 .016 261.71	.052-LOWER CP-MAG PHI	5.000 204.81 .660 309.72 .166 104.10 .148 21.00 .099 251.56 .059 198.75 .059 198.75	.800-LOWER CP-MAG PHI	422 10.09 559 23.34 559 23.34 559 23.34 559 53.55 110 253.55 613 103.65 602 322.02 602 322.02
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OCWI PE ODE 1 CENTER 15 ALPHA-FCL 31 ALPHA-PEL 1 SIGWA COMPUTED FPERUE UDE AND PHASE AN	.146-UPPFR CP-FAG PHI	3.375 195.91 .340 23.20 .307 23.20 .102 15.29 .152 248.11 .154 254.88 .634 265.11	.910-UPPER CP-MAG PHI	1.071 117.92 .423 19.06 .423 19.06 .081 39.94 .038 39.24 .176 246.44 .545 191.82 .633 244.8 .610 273.36	.6t1-LOWER CP-MAG PHI	1.035 47.40 323 40.40 634 25.25 643 31.35 045 35.35 118 252.38 636 232.57 605 148.59
MC FILE 1 RUN POINT SSURES, PER PADI	.062-UPPER CP-MAG PHI	5.443.7.10.00.00.00.00.00.00.00.00.00.00.00.00.	. 560-UPPER CP-MAG PHI	1.273 119.17 1.435 25.66 2.5 66 1.6 1 46.22 1.2 9.20 1.0 1.2 9.20 1.0 1.2 9.20 1.0 1.2 9.20 1.0 1.2 9.20 1.0 1.3 7.25 1.0 1.3 7.25 1.0 1.3 7.25 1.0 1.3 7.25 1.0 1.3 7.3 1.0	.53C-LOWER	1.711 38.86 313 12.33 12.33 12.33 12.45 12.45 12.4 24 12.4 24 12.4 25 12.4 25 14.1 24 16.1 24
FOURTER COEFF	CP-MAG PHI	25.559 195.11 2.4373 100.23 2.4379 235.52 3.839 255.65 3.85 203.63 1.85 203.63 1.11 24.62 1.54 165	= .774-UPPER CP-MAG PHI	1.554 123.95 446 365.95 683 43.95 646 493.78 124 249.77 1045 109.77 1015 257.60	= .392-LOWER CP-MAG PHI	1.634 .2334 .313 .631 .631 .632 .635 .635 .635 .635 .635 .635 .635 .635
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15b ALPHA-PR 31 ALPHA-PA CO*FUTED FPECU UDE AND PHASE A FORCE, AND MOME	DELCPM PHI	7.664 18.72 268 224.81 067 190.70 658 124.75 616 13.75 015 207.71 045 156.67 017 33.70 027 330.96	DELCPM PHI	.357 331-01 .182 185-79 .006 291-72 .007 38-46 .009 27-99 .009 129-92 .006 338-92 .005 338-92	AN COR		648 20153 1112 205.68 1012 205.68 1012 205.68 2010 2010 2010 2010 2010 2010 2010 201
FILF RUN POINT ICILNIS, AMPLITA SSURES, NORMAL	DELCP# 562 PHI	11.265 17.41 799 204.16 346 127.041 1051 248.96 1056 174.91 1029 57.60 1042 367.26	BELCP PAI	735 330 74 0146 259 74 0146 199 73 015 140 53 012 337 34 012 151 68 015 152 01 0015 359 87	SURES, PER HADI	#1 125 AG FHI CP-	244 358 358 258 258 251 251 251 251 251 251 251 251
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OCWIEPBLE ALPHA-WCL ALPHA-PCL ALSIGWA = 1 UZEU FREQUENCY ND PHASE ANGLE	•148 PM PHI DEL	55.256.39 56.213.68 36.191.23 37.78.70 37.78.70 37.78.70 38.79.70 38.79.70 39.79.70 30.19.79 30.19.73	•910 PM PHI	10 161 86 10 161 86 10 255 88 10 255 88 10 255 89 10 15 79 10 196 88	#	H4 *125 PHI CP-HAG	22.89 13.586 1.546 149.92 77.53 77.53 15.99 15.99 15.99 15.99 15.99 15.99 15.99 15.99 15.99
MODE 1 FILE 134 RUN 35 POINT COMP	S, NORMAL FORC D62 PM PHI DEL	53 355.99 61 232.46 52 22.26 52 26.35 52 26.35 50 1 40.64 50 1 129.65 51 108.29	PR PHI DELC	441 252.82 1.3 252.46 1.1 252.46 1.1 293.82 1.0 0.0 0.5 299.67 1.0 0.0 0.4 1.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	PER RADIAN **	WZ • JUG PHI CP-MAG	12.37 54.75 54.65 54.65 51.97 64.50 6014 69.77 69.77 69.77 69.77
NIER COLFFICIEN BLADE PRESSURE	.012 H PHI DELC	2 255.56 14.3 2 257.24 1.1 2 315.70 3 10.4 3 10.4 4 227.97 7 295.77	774 PHI DELC	1.255 2.	WALL PRESSURES	10N -1255 N CP-MAG	2 2 4 4 5 2 4 4 5 5 5 5 5 5 5 5 5 5 5 5
7.4 0.4 7.4 8.4	X = N DELCP	33. 34. 34. 34. 34. 34. 34. 34. 34. 34.	X = DELCP	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	*	BALL NO	